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MULTIVARIATE NORMAL INTEGRATION

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Multivariate Normal Distribution
Statistical Analysis
Monte Carlo Methods

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1. Introduction

This paper presents the results of an investigation into the application of the Monte Carlo integration technique in the evaluation of multivariate normal (MVN) integrals. Specifically the theory and resultant computer program is developed to evaluate MVN integrals for the following situations:

- Over rectangular areas for dimension M < 5
 utilizing completely arbitrary input parameters
 (mean vector and variance-covariance matrix) and
- 2) Over elliptical regions for arbitrary bivariate normal densities.

Section 2 presents pertinent results on the MVN distribution and describes the Monte Carlo technique in general applications. Section 3 presents the theory pertinent to our particular applications and section 4 discusses specific applications. The appendix presents the computer program and discusses the preparation of input cards.

2. General Theory

The Monte Carlo technique is, in general, a random simulation of a deterministic process. In integral evaluation one numerically evaluates a quantity whose expected value is the value of the integral and we can apply those statistical tech-

niques applicable to such procedures.

The general principles of Monte Carlo procedures are well documented. The texts by Shreider (1964) and Newman and Odell (1971) provide excellent discussions on the Monte Carlo technique of integration.

As a simple, and inefficient, example consider the integral

$$\theta = \int_0^1 x \, dx.$$

Suppose we desire to evaluate the integral

$$\theta = \int_{R_{\underline{m}}} f(\underline{x}) g(\underline{x}) d\underline{x}. \tag{1}$$

where $g(\underline{x})$ denotes a probability density function on R_m . The integral (1) is then merely the expected value of the function f(x) and can be estimated by evaluating the quantity

$$\hat{\theta} = \frac{1}{N} \sum_{i=1}^{N} f(\underline{x}_i)$$

where \underline{x}_i , i=1, N, are samples from the pdf $g(\underline{x})$. We directly have

$$\operatorname{Var}(\hat{\theta}) = \frac{1}{N} \operatorname{Var}(f(\underline{x})) = \frac{1}{N} \int_{R_m} (f(\underline{x}) - \theta)^2 g(\underline{x}) d\underline{x}$$

which is estimated by the quantity

$$s^{2} = \frac{1}{N-1} \sum_{i=1}^{n} (f(\underline{x}_{i}) - \hat{\theta})^{2}$$

giving an estimated standard error of $\hat{e} = S/\sqrt{N}$. This quantity can be used to put confidence intervals on θ by the standard method.

One useful way to reduce the magnitude of $Var(\hat{\theta})$ and, consequently, S^2 is to "remove the regular part". Suppose there exists a function $h(\underline{x})$ on R_m that approximates $f(\underline{x})$ well on R_m and further suppose that the value

$$\Psi = \int_{R_{\underline{m}}} h(\underline{x}) d\underline{x}$$

is known. We then have

$$\theta = \Psi + \int_{R_{\underline{m}}} (f(\underline{x}) - h(\underline{x})) d\underline{x}.$$
 (2)

The variance of $f(\underline{x}) - h(\underline{x})$, where \underline{x} has pdf $g(\underline{x})$, is

$$Var(f(\underline{x})-h(\underline{x})) = Var(f(\underline{x})) + Var(h(\underline{x})) - 2 Cov(f(\underline{x}),h(\underline{x}))$$

and if $Var(h(\underline{x})) < 2 Cov(f(\underline{x}), h(\underline{x}))$ we have immediately the result that

$$Var(f(\underline{x})-h(\underline{x})) < Var(f(\underline{x})).$$
 (3)

The MVN distribution is well documented and this discussion is merely to introduce notation and present results to be used in section 3.

The MVN density is the expression

$$f(\underline{\mathbf{x}}|\underline{\mu},\Sigma) = \frac{1}{\frac{\underline{\mathbf{m}}}{(2\pi)^2|\Sigma|}} e^{-1/2(\underline{\mathbf{x}}-\underline{\mu})^2\Sigma^{-1}(\underline{\mathbf{x}}-\underline{\mu})}$$

where $\underline{\mu}$ is the vector of means and Σ is the positive definite, symmetric variance-covariance matrix. For such matrices there always exists a lower triangular matrix A such that $\Sigma = AA'$. Immediately we have $|\Sigma| = |A||A'| = |A'|^2$ giving $|\Sigma|^{1/2} = |A'|$ and, as A' is upper triangular, |A'| is the product of the diagonal elements of A. If we define a linear transformation $\underline{Y} = (A^{-1})'(\underline{x}-\underline{\mu})$ then $\underline{Y}'\underline{Y} = (\underline{x}-\underline{\mu})'A^{-1}(A^{-1})'(\underline{x}-\underline{\mu}) = (\underline{x}-\underline{\mu})'\Sigma^{-1}(\underline{x}-\underline{\mu})$. This result yields the equivalent pdf

$$g(\underline{y}) = \frac{1}{(2\pi)^{\frac{m}{2}}} e^{-1/2\Sigma y_{\underline{i}}^2}$$

Thus by a suitable linear transformation any MVN pdf can be reduced to the product of independent standard normal variates.

These results are utilized in our computer program.

Specific Results

This section is divided into two parts; the first dealing with the algorithm for integration over rectangular regions and the second dealing with integration over elliptical areas in the bivariate case.

3.1 Integration Over Rectangular Areas

Suppose we desire to evaluate the integral

$$\theta = \int_{a_1}^{b_1} \int_{a_2}^{b_2} \dots \int_{a_m}^{b_m} f(\underline{x} | \underline{\mu}, \Sigma) dx.$$
 (5)

Referring to formula (1) we define $g(\underline{x}) = 1/\prod_{i=1}^{m} (b_i - a_i)$ and evaluate the integral

$$\phi = \int_{a_1}^{b_1} \int_{a_2}^{a_1} \dots \int_{a_m}^{b_m} f(\underline{x} | \underline{\mu}, \Sigma) \underbrace{\frac{dx}{m}}_{i=1} (b_i - a_i)$$

and observe that we have

$$\theta = \phi \prod_{i=1}^{m} (b_i - a_i), \qquad (6)$$

and the estimate

$$\hat{\theta} = \hat{\phi} \prod_{i=1}^{m} (b_i - a_i),$$

where

$$\hat{\phi} = \frac{1}{N} \Sigma f(\underline{x}, |\underline{\mu}, \Sigma)$$

when $\underline{\mathbf{x}}_{\mathbf{i}}$ is a random vector from the pdf

$$g(\underline{x}) = \begin{cases} \frac{1}{m} & \text{if } i \leq x_i \leq b_i, i=1, m. \\ i = 1 & \text{otherwise} \end{cases}$$

This result is deceptively simple. The pdf $g(\underline{x})$ is the product of m independent uniform distributions and a random

vector is generated using the equations $x_i = a_i + u_i (b_i - a_i)$, i = 1, m, where u_i is a usual [0,1] random number.

In the program we obtain the $\Sigma = AA'$ factorization and calculate A^{-1} and |A'|. The algorithm proceeds to calculate \underline{x} , $\underline{y} = (A')^{-1}(\underline{x}-\underline{\mu})$ and $\underline{y}'\underline{y}$. Then $f(\underline{x}|\underline{\mu},\Sigma)$ follows directly.

This procedure converges slowly in most cases and an effort to increase the precision and speed of convergence was attempted by "removing the regular part" as generally described in section 2. Basically it consisted of expanding the expression

 $-1/2(x-\mu)\sum^{-1}(x-\mu)$ into a Taylor's series and defining h(x) as the first three terms. The arithmetic is formidable and not germane to subsequent discussions. Consequently, it will not be presented in the text but can be obtained from the appended computer program.

The function $h(\underline{x})$ described above effectively decreases the standard error of the estimate when the integration ranges are small. To determine precisely where $h(\underline{x})$ fails, i.e., where $Var(h(\underline{x})) > 2 Cov(f(\underline{x}))$ is a formidable task and not really necessary. To utilize this approach the computer must perform the calculations to evaluate (5) using the standard approach - the difference being the number of random number generations required to attain a specified level of the standard error of estimation (program input). At each 100 generations we check both errors and if either is below the specified level the computations terminate with the answer, standard error and an indication whether or not the regular part

was removed being printed.

3.2 Elliptical Regions

This portion of the program has more direct applications to meteorological problems as the examples in the next section will show.

The general procedure is very similar to the case in section 3.1. Assuming we desire to integrate the bivariate normal pdf over an elliptical region E having area Nab where a and b are axis lengths, i.e., we desire to evaluate

$$\theta = \int_{\mathbf{E}} f(\underline{\mathbf{x}} | \underline{\mu}, \Sigma) d\underline{\mathbf{x}}. \tag{7}$$

Defining $g(x) = 1/\mathbb{I}ab$ we evaluate

$$\phi = \int_{E} f(\underline{x} | \underline{u}, \Sigma) d\underline{x} / \Pi ab$$

and, analogous to (6) above, obtain

$$\theta = \phi \text{ Nab.}$$

Here, as above, the problem is to generate a series of random vectors in the region being integrated over. The general procedure is to assume the ellipse is in standard position, i.e.,

ES =
$$\{(x,y) | \frac{x^2}{2} + \frac{y^2}{2} \le 1\}$$
, obtain a random point in this ellipse and rotate and/or translate it to the area E. This random point

in ES is obtained by generating two uniform [0,1] numbers u_1 and u_2 . The equations $x = a(1-2u_1)$ and $y = b\sqrt{1-x^2/a^2}$ (1-2u₂) determine a random point on ES. Once

translated and/or rotated to E the method in 3.1 applies except there is no provision for removing the regular part.

Program input permits considerable flexibility in the elliptical parameters required. Specifically, there are two options:

- 1) Inputs include x, y axis lengths, rotation angle and center after rotation or
- 2) Input 5 points on the locus of an ellipse (the program determines the ellipse and puts it in standard form).

4. Applications

This section presents some general numerical results and some examples. Specifically we present program outputs utilizing the data in Crutcher (1967). This also permits comparisons of our probabilities with those obtained by using the Cornell Aeronautical Laboratory tables (Groenewoud, et.al., 1967) on bivariate normal integrals over elliptical regions. We will, however, first present some computations over rectangular regions. The accuracy of our computations can be easily ascertained as they are merely products of independent standard normal integrals. Tables 1-4 present, respectively, the computations for the integrals

1.
$$\int_{0}^{1} f(x|0,1) dx,$$

3.
$$\int_0^1 \int_0^1 f(\underline{x}|\underline{0},I) d\underline{x}$$

and

4.
$$\int_0^1 \int_0^1 \int_0^1 f(\underline{x}|\underline{0},I) \ d\underline{x}.$$

The correct answers, using the normal probability tables in the C.R.C. Standard Mathematical Tables (Weast, 1968) are written in below the value calculated by the program.

TABLE 1

MULTIVARIATE NORMAL INTEGRAL

THE VECTOR OF MEANS IS

THE RANDOM NUMBER IS 5423

THE STANDARD ERROR IS LESS THAN 0.00100000

THE VARIANCE - COVARIANCE MATRIX S IS

1.00000	0.00000	0 . 00 00	0.00000	0.00000
0.00000	0.0000	0.00006	0.00000	0.00000
0.00000	0.00000	0.0000	0.00000	0.00000
3.30396	_ <u>0.00</u> 000	o.0000c	0.00000	0.00000
0.00000	0.00000	0.00000	0.00000	0.00000

UPPER TRIANGULAR FACTORIZATION

1.00000

INVERSE OF A TRANSPOSE

1.00000

INVERSE OF S

1.00000

FOR RECTANGULAR REGION DIMENSION = 1

THE LOWER INTEGRATION LIMITS ARE

THE UPPER INTEGRATION LIMITS ARE 1.0000002

THE VALUE IS 0.3412368 WITH A STANDARD ERROR OF 0.0001802

THE REGULAR PART HAS BEEN EXTRACTED

THE CORRECT VALUE IS .341345

MULTIVARIATE NORMAL INTEGRAL

THE VECTOR OF MEANS IS

THE RANDOM NURBER IS 8135

THE STANDARD ERROR IS LESS THAN 0.00100000

THE VARIANCE - COVARIANCE MATRIX 5 IS

1.00000	0.00000	0.00000	0.00000	0.00000
0.00000	1.00000	0.0000	0.00000	0.00000
0.00000	0.00000	0.0000	0.00000	0.00000
0.0000	0.00000	0.00000	0.0000	0.00000
0.00000	0.00000	0.00000	0.00000	0.00000

UPPER TRIANGULAR FACTORIZATION

1.00000 0.00000 0.00000 1.00000

INVERSE OF A TRANSPOSE

1.00000 0.00000 0.00000 1.00000

INVERSE OF S

0.00000 1.00000 0.00000 1.00000

FOR RECTANGULAR REGION DIMENSION = 2

THE LOWER INTEGRATION LIMITS ARE

-1.0000002

-1.00000002

THE UPPER INTEGRATION LIMITS ARE

1.00000002

1.0000002

THE VALUE IS 0.4668157 WITH A STANDARD ERROR OF 0.0009669

AND A CORRELATION OF 0.8419297

THE REGULAR PART HAS BEEN EXTRACTED

THE CORRECT VALUE IS .46607

YULTIVARIATE NORMAL INTEGRAL

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Ţ	HE	RAND)O:// N	ب ۱۹۹۷	<u>२</u> ।	5	9631				
T	HE	STAN	.DARD	ER	CR	I5	LES S	THAN	0.0	0010000	0
T	μĘ	∀४२1	ANCE	- (AVC	RIA	NCE	MATRIX	SI	S	

1.00000	0.00000	0.00000	0.0000	0.00000
0.00000	1.00000	J.JJJJD	0. 00000	0.00000
0.00000	0.000 0 0	1.00000	0.00000	0.00000
o.00000	0.0000 0	0.00000	3. 00000	0.00000
0.00000	0.00000	0.00000	0.00000	0.00003

UPPER TRIANGULAR FACTORIZATION

_1.00000	0.00000	.5.00000
0.30000	1.00000	ე. ეიეიე
0.00000	0.0000	1.00000

INVERSE OF A TRANSPOSE

1.00000	0.0000	0.00000
0 .000 00	1.00000	0.00000
0.00000	0.00000	1.00000

INVERSE OF S

1.05600	0.00000	0.00000
0.00000	1.00000	0.0000
0.00000	0.00000	1.00000

FOR RECTANGULAR REGION DIMENSION = 3

THE LOWER INTEGRATION LIMITS ARE

J.0000000

0.3366**6**

0.0000000

THE UPPER INTEGRATION LIMITS ARE

1.0000002

1.0000002 1.0000002

THE VALUE IS 0.0397351 WITH A STANDARD ERROR OF 0.0002741

AND A COPRELATION OF 0.8054759

THE REGULAR PART HAS BEEN EXTRACTED

THE CORRECT VALUE IS .039772

MULTIVARIATE NORMAL INTEGRAL

THE VECTOR OF 0.0000000	0.0000000	0.000	000 0	0.000000	
THE BANKS					
THE RANDOM NUM	BER IS 7317				
THE STANDARD E	२२०२ IS LESS	THAN 0.001	00000		
THE VARIANCE -	COVARIANCE M	ATRIX S IS		· · · · · · · · · · · · · · · · · · ·	
1.00000	0.00000		_		
7.00000	1.00000	0.00000	0.00000		
0.00000	0.00000	0.00000	0.00000	*******	
0.00000	0.00000	1.00000 0.00000	0.00000		
0.00000	0.0000	3.0000	1.00000		
		3.33000	0.0000	0.0000	
UPPER TRIANGUL	AR FACTORIZAT	ION	·		
1.00000	J.00000	0.00000	0 0000		
0.00000	1.00000	0.00000	0.00000		
0.00000	0.00000	1.00000	0.00000		
0.00000	0.00000	0.00000	0.00000		
1.00000 0.00000 0.00000 0.00000	0.00000 1.00000 0.00000	0.00000 0.00000 1.00000	0.00000 0.00000 0.00000		
	0.00000	0.00000	1.00000		
INVERSE OF S					
1.00000	<u>0.00000</u>	0.00000	0.0000		
0.00000	1.00000	0.0000	0.00000		
0.00000	0.00000	1.30000	0.00000		
0.00000	0.00000	0.00000	1.00000		
	FOR RECTA	NGULAR REGI	ONDIMENS	1014 = 4	
THE LOWER INTEG	RATION LIMITS	ASE			
0.0000000	0.0000000	0.0000	000	0.000000	
HE UPPER INCHES	OATTON TO				
THE UPPER INTEG	1.0000002				
	_	1.0000		1.0000002	
HE VALUE TS TO	0135361 WITH	A CTABILITY			

The output is self-explanatory except for the standard error value. The value .001 is used in each case. This quantity is the standard error of the estimated integral value. In Table 1 the estimated value is .341236 with a standard error of .00018 and, consequently, a 95% confidence interval on the "true" value of the integral is .341236 ± .00035 which is observed to contain the true value in this case.

The above paragraph demonstrates the basic statistical approach of the Monte Carlo technique. We are estimating a parameter in the strictest sense and this estimate has the same validity of an estimate for any quantity when many samples (likely several thousand in most cases) are involved. Here, as in most applications, the well-known mechanism of increasing the precision by increasing the sample size and/or decreasing the population variance (as the "regular part" does in some instances) is working. The confidence placed in these numbers should be no more or no less than the confidence placed in the results of any carefully designed, controlled and extensive sampling scheme.

The next three tables (5-7) present the calculated probabilities for examples H, I and J (pp. 25-31) in Crutcher (1967). Briefly, the examples are presented below:

Example H: 24-Hour Displacement of Asiatic East Coast

Cyclones Originating East of 130° East Longitude.

Bivariate Normal Parameters (Units in latitude)

$$\bar{x} = 8.9$$
 $S_x = 3.10$ $r_{xy} = .292$

$$\bar{y} = 4.6$$
 $S_y = 3.70$

The problem is to evaluate the probability of observing a cyclone after 24-hours in a circle centered due east of the original position at a distance of 8 degrees of latitude with a radius of 2 degrees.

Example I: Upper Wind Velocities for January at 6 km above Greensboro, North Carolina.

Bivariate Normal Parameters (Units are meters/sec. with winds from south and west positive)

$$\bar{x} = 24.04$$
 $S_x = 13.12$ $r_{xy} = .174$ $\bar{y} = 1.22$ $S_y = 12.65$

The problem is to evaluate the probability of observing winds at 6 km equal to or less than 5 meters/sec.

Example J: 36-Hour Displacement of Tropical Storms.

Bivariate Normal Parameters (Units are degrees of latitude)

$$\bar{x} = -2.9$$
 $S_x = 3.87$ $r_{xy} = .581$ $\bar{y} = 3.9$ $S_y = 2.30$

The problem is to evaluate the probability of observing a storm within 2 degrees latitude of a point (-5.0, 5.0) from the storm center 36 hours previously.

On each table the probability obtained by using the Cornell Tables and the exact calculated probability, furnished by Crutcher (1967), are given.

'ALLE T	TWARTATE	NORMAL	INTEGRAL
CULI	TANKTHIE	NURMAL	THIERWAL

THE VECTOR OF MEANS IS 8.9000015 4.6000003

THE RANDOM NUMBER IS 3527

THE STANDARD ERROR IS LESS THAN 0.00100000

THE VARIANCE - COVARIANCE MATRIX 5 15

9.61000	3.34923	0.0000	0.0000	0.00000
3.34923	13.68999	0.0000	0.00000	0.00000
0.00000	0.0000	0.0000	0.00000	0.00000
0.00000	0.00000	0.00000	0.00000	0.00000
0.00000	0.00002	0.00000	0.30000	0.00000

UPPER TRIANGULAR FACTORIZATION

3.09999 1.08039 0.0000C 3.53874

INVERSE OF A TRANSPOSE

0.32258 0.00000 -0.09848 0.28258

INVERSE OF 5

0.11375 -0.02783 -0.02783 0.07985

FOR BIVARIATE ELLIPTICAL REGION

THE ROTATION ANGLE IS 0.00000

THE X AND Y AXIS LENGTHS ARE 2.0000 2.0000 THE CENTER AFTER ROTATION IS 8.0000 0.0000

THE VALUE IS 0.0783936 WITH A STANDARD ERROR OF 0.0009339

VALUE USING CORNELL TABLES IS .07733

EXACT CALCULATED VALUE IS .07713

MULTIVARIATE	NORMAL	INTEGRAL
--------------	--------	----------

THE VECTOR OF MEANS IS 24.0400009 1.2200000

THE RANDOM NUMBER IS 1179

THE STANDARD ERROR IS LESS THAN 0.00100000

THE VARIANCE - COVARIANCE MATRIX S IS

172.13439	28.87842	0.0000	0.00000	0.00000
28.87842	160.02249	0.00000	0.00000	0.00000
0.00000	0.0000	0.0000	0.00000	0.00000
0.00000	0.00000	0.0000	0.00000	0.00000
0.00000	0.0000	2.22000	0.00000	0.0000

UPPER TRIANGULAR FACTORIZATION

13.11999 2.20110 0.00000 12.45703

INVERSE OF A TRANSPOSE

0.07621 0.00000 -0.01346 0.08027

INVERSE OF S

-0.00599 -0.00108 -0.00108 0.00644

FOR BIVARIATE ELLIPTICAL REGION

THE ROTATION ANGLE IS 0.00000

THE X AND Y AXIS LENGTHS ARE 5.0000 5.0000
THE CENTER AFTER ROTATION IS 0.0000 0.0000

THE VALUE IS 0.0146852 WITH A STANDARD ERROR OF 0.0006107

VALUE USING CORNELL TABLES IS .01474

EXACT CALCULATED VALUE IS .01431

TABLE 7

ZULTIVAR	IATE	NORMAL	INTEGRAL
----------	------	--------	----------

THE VECTOR OF MEANS IS -2.9000001 3.9000001

THE RANDOM NUMBER IS 2399

THE STANDARD ERROR IS LESS THAN 0.00100000

THE VARIANCE - COVARIANCE MATRIX 5 IS

14.97690	5.17148	0.30000	0.00000	0.00000
5.17148	5.29999	0.00000	J.00000	0.00000
D.0000U	0.00000	0.0000	0.00000	0.0000
0.00000	6.00000	0.00000	0.00000	0.00000
0.00000	0.00000	0.00000	0.00000	C.00000

UPPER TRIANGULAR FACTORIZATION

3.86999 1.33629 C.0000C 1.87197

INVERSE OF A TRANSPOSE

0.25839 0.00000 -0.18445 0.53419

INVERSE OF S

0.10079 -0.09653 -0.09853 0.28536

FOR SIVARIATE ELLIPTICAL REGION

THE ROTATION ANGLE IS 0.00000

THE X AND Y AXIS LENGTHS ARE 2.0000 2.0000 THE CENTER AFTER ROTATION IS -5.0000 5.0000

THE VALUE IS 0.1445387 WITH A STANDARD ERROR OF 0.0009946

VALUE USING CORNELL TABLES IS .14363

EXACT CALCULATED VALUE IS .14546

The Monte Carlo technique is a technique of considerable value in evaluating complicated integrals. From the two cases presented here the reader can readily grasp the importance of a proper selection of the pdf $g(\underline{x})$. If the region being integrated over can be described mathematically the process is readily applicable – the form of the integrand presents no problem if it can be evaluated accurately.

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Appendix

This appendix provides a detailed description of the required card inputs to utilize the programs, along with appropriate JCL for the computer being utilized. The programs are written in Fortran IV.

The changes necessary to adapt the program to a specific computer will be the modification to utilize a random number generator other than the IBM SSP routine called RANDU and assigning the proper logical unit numbers to reader and printer. The former can be accomplished by changing Format statement number 90 to conform to prescribed starting integer length (presently the variable designation is Ix read in I4 format) and the latter can be accomplished by changing the R=2 and P=3 cards at the beginning of the program to designate the reader and printer logical numbers.

Description - Card Input

COL.

- CARD 1 1 DIMENSION OF INTEGRAL
 - 2 0 = RECTANGULAR INTEGRATION, 1 = ELLIPSE
 - 3 0 = INPUT IS X & Y AXIS LENGTHS, ROTATION ANGLE &

CENTER AFTER ROTATION

- 1 = INPUT IS 5 POINTS ON ELLIPSE
- 4-7 4 DIGIT RANDOM NUMBER (LAST DIGIT ODD)
- 8-17 MAXIMUM STD ERROR OF THE MEAN PERMITTED (F10.6 FORMAT)

CARD 2 VECTOR OF MEANS (MAXIMUM OF 5) 5F8.3 FORMAT

- CARDS 3 lst CARD FIELD 1 COLS 1-8 STD DEVIATION OF 1st VARIABLE to 3+N-1
 - 2 9-16 CORRELATION OF 1st & 2nd VARIABLE
 - 3 17-24 CORRELATION OF 1st & 3rd VARIABLE
 - 4 25-32 CORRELATION OF 1st & 4th VARIABLE
 - 5 33-40 CORRELATION OF 1st & 5th VARIABLE
 - 2nd CARD FIELD 1 COLS 1-8 STD DEVIATION OF 2nd VARIABLE
 - 2 9-16 CORRELATION OF 2nd & 3rd VARIABLES
 - 3 17-24 CORRELATION OF 2nd & 4th VARIABLES
 - 4 25-32 CORRELATION OF 2nd & 5th VARIABLES

3rd CARD etc.

- NOTE: THERE WILL BE AS MANY CARDS AS THE DIMENSION OF THE INTEGRAL EACH CARD CONTAINING THE STD DEVIATION OF A VARIABLE AND
 CORRELATIONS WITH SUCCEEDING VARIABLES WITH 1st CARD DEVOTED
 TO VARIABLE 1, 2nd CARD TO VARIABLE 2, ETC.
 - IF CARD 1, COL 2 = 0

THE NEXT TWO CARDS CONTAIN THE LIMITS OF INTEGRATION

THE FIRST CONTAINING THE LOWER LIMITS, THE SECOND CONTAINING THE UPPER LIMITS. BOTH CARDS HAVE 5F8.3 FORMATS.

- 1st CARD FIELD 1 COLS 1-8 LOWER INTEGRATION LIMIT ON VARIABLE 1
 - 2 9-16 LOWER INTEGRATION LIMIT ON VARIABLE 2
 - 3 17-24 LOWER INTEGRATION LIMIT ON VARIABLE 3
 - 4 25-32 LOWER INTEGRATION LIMIT ON VARIABLE 4
 - 5 33-40 LOWER INTEGRATION LIMIT ON VARIABLE 5
- 2nd CARD FIELD 1 COLS 1-8 UPPER INTEGRATION LIMIT ON VARIABLE 1
 - 2 9-16 UPPER INTEGRATION LIMIT ON VARIABLE 2
 - 3 17-24 UPPER INTEGRATION LIMIT ON VARIABLE 3
 - 4 25-32 UPPER INTEGRATION LIMIT ON VARIABLE 4
 - 5 33-40 UPPER INTEGRATION LIMIT ON VARIABLE 5

IF CARD 1, COL 2 = 1

THE NEXT CARD CONTAINS ELLIPSE INFORMATION

IF CARD 1, COL 3 = 0

- FIELD 1 COLS 1-10 ROTATION ANGLE IN RADIANS F10.3 FORMAT
 - 2 11-20 X AXIS LENGTH (in regular position) F10.3 FORMAT
 - 3 21-30 Y AXIS LENGTH (in regular position) F10.3 FORMAT
 - 4 31-40 X COORDINATE OF CENTER F10.3 FORMAT
 - 5 41-50 Y COORDINATE OF CENTER F10.3 FORMAT
- IF CARD 1, COL 3 = 1
 - FIELD 1 COLS 1-6 X COORDINATE OF 1st POINT
 - 2 7-12 Y COORDINATE OF 1st POINT F6.2 FORMAT
 - 3 13-18 X COORDINATE OF 2nd POINT F6.2 FORMAT
 - 4 19-24 Y COORDINATE OF 2nd POINT F6.2 FORMAT
 - 5 25-30 X COORDINATE OF 3rd POINT F6.2 FORMAT

31-36 Y COORDINATE OF 3rd POINT F6.2 FORMAT

37-42 X COORDINATE OF 4th POINT F6.2 FORMAT

43-48 Y COORDINATE OF 4th POINT F6.2 FORMAT

49-54 X COORDINATE OF 5th POINT F6.2 FORMAT

55-60 Y COORDINATE OF 5th POINT F6.2 FORMAT

```
DIMENSION X(5),S(5,5),A(5),B(5),E(5,5),H(5,5),Y(5),SD(5),RHO(5,5),
     1KN 50 9K((5) 9F(5+5) 9U(5) 9AXIS(2) 9PTS(2) 9AX(2) 9AY(2) 9XBR(5)
C
      704 MA 733 (1.14.F10.6)
   91 704/47,578.31
   93 FORM TO DITHE VARIANCE - COVARIANCE MATRIX S IS'/)
      TO HITE AND AND INPUT PARAMETER!)
0.3
      FORWACIANT LOSS OF SIGNIFICANCE!)
45
      FORMS (//, UPPER TRIANGULAR FACTORIZATION './)
95
            13.5(2X.F10.5))
0.7
      FORMACCE, INVERSE OF A TRANSPOSE' . /)
9.8
      FORMATIMATI INVERSE OF S!+/)
99
      FORWATE COTHE VALUE IS', F15.10. WITH A STANDARD ERROR OF', F15.10./
100
     IN THE VALUE IS CALCULATED WITHOUT REMOVING THE REGULAR PART!)
     FORMATHIOTHE VALUE IS', F15.10, WITH A STANDARD ERROR OF', F15.10.
     1 AND A CORPELATION OF *F15.10.//! THE REGULAR PART IS POSITIVELY C
     20RRELATED WITH THE INTEGRAL AND IS THUS EXTRACTED!)
C
      EPS=,000001
1
      CONTINUE
      00 112 I=1.5
      00 112 J=1.5
  112 5(I:J)=0.
      5-RITE(3+8)
    8 FORMATI'1',20X,29HMULTIVARIATE NORMAL INTEGRAL /)
      READ(2+90) N+KODE+1CODE+1X+ERROR
      READ(2,91) (U(1), I=1,N)
      00 2 L=1.N
      LL=L+1
      READ(2,91) SD(L) + (RHO(L+K) + K=LL+N)
      WRITE(3,105) (U(I),I=1,N)
  105 FORMAT( OTHE VECTOR OF MEANS IS 1/.1x.5(F12.7.3X))
      WRITE(3,107) IX, ERROR
      FORMATI//, THE RANDOM NUMBER IS', 16// ' THE STANDARD ERROR IS LES
     15 THAN ' > F12.8)
      DO 3 I=1.N
      LL=[+]
      S(I,I)=SD(I)**2
      DO 3 L=LL.N
      S(I,L)=RHO(I,L)*SD(I)*SD(L)
3
      S(L,I)=S(I.L)
      WRITE (3,93)
      00 4 1=1.5
      WRITE(3,97) (S(1,J),J=1,5)
    FACTOR MATRIX S
      DO 10 I=1.N
      DO 10 J=1.N
      E(:,J)=S(I,J)
10
      H(I+J)=S(I+J)
      CALL ARRAY(2+N+N+5+5+E+E)
      CALL MSTR(E.F.N.O.1)
      CALL VISD (F.N.EPS.IER)
      CALL MSTR(F.E.N.1.0)
      CALL ARRAY(1,N,N,5,5,E,E)
      IF (N-1) 11.13.11
11
      NN=N-1
      DO 12 J=1,NN
                                       26
```

```
IFH=J+1
      DC 12 I=IFH.N
12
      E(I,J)=0.0
13
      IF(IER) 14,16,15
14
      WRITE(3,94)
      GO TO 16
15
      WRITE(3,95)
      WRITE(3,96)
      DO 17 I=1.N
17
      WRITE(3,97) (E(I,J),J=1,N)
C
    INVERT A
C
      DO 18 I=1.N
      DO 18 J=1.N
18
      F(J,I)=E(I,J)
      CALL ARRAY(2+N+N+5+5+F+F)
      CALL MINV(F.N.DU.KN.KI)
      CALL ARRAY(1.N.N.5.5.F.F)
      IF(IER) 19,21,20
19
      WRITE(3,94)
      GO TO 21
20
      WRITE(3,95)
21
      WRITE(3,98)
      DO 22 I=1.N
22
      WRITE(3.971-1P(1.J)
      CALL ARRAY(2+N+N+5+5+H+H)
      CALL MSTR(H.S.N.O.1)
      CALL SINV(S,N,EPS, IER)
      CALL MSTR(S+H+N+1+0)
      CALL ARRAY(1.N.N.5.5.H.H)
      IF(IER) 23,25,24
23
      WRITE(3,94)
      GO TO 25
24
      WRITE(3,95)
25
      WRITE(3,99)
      DO 26 I=1,N
26
      WRITE(3+97) (H(1+J)+J=1+N)
C
C
    CALCULATE CONSTANT C
      PROD=1.
      DO 30 I=1.N
      PROD=PROD*E(I.I)
      PPROD=PROD**2
      C=((6.283185307)**N*PPROD)**(-.5)
      IF(N-2) 32,31,32
C
C
    IF KODE = 1, THIS IS AN ELLIPSE
31
      IF(KODE) 32,32,200
C
C
    CALCULATE QUANTITY Q
   32 WRITE(3,111)N
  111 FORMAT(21X, FOR RECTANGULAR AREA, DIMENSION = 1,12/)
```

```
343E 3
      21=1,
      7547(7.91) (A(I).I=1.N)
      RE40(2,91) (B(I),I=1,N)
      ARITE(3+105) (A(I)+I=1+N)
               THE LOWER INTEGRATION LIMITS ARE! / . 1X . 5 (F12 . 7 . 3X))
      wR178(3:108) (B(I):I=1:N)
  108 FORMETI OTHE UPPER INTEGRATION LIMITS ARE! / . 1X . 5 (F12 . 7 . 3X ))
            <u> :=i+A</u>
      P1=P1*(B(I)-A(I))
33
      30 36 I=1.N
      DIF1=(8(1)-U(1))**3-(A(1)-U(1))**3
      TE2=(F:1)-U(1))**5-(A(1)-U(1))**5
      P2=1.
      DO 35 J=1.N
      IF(U-1)34,35,34
   34 P2=72#(B(J)-A(J))
   35 CONTINUE
      SUM1=SUM1+(H(I+I)*DIF1*P2)
   36 TS1=TS1+(H(I,1)**2*TE2*P2)
      SUM1=(-.5)*SUM1/3.
      TE1=.025*TS1
      SUM2=0.0
      IF(N-1) 42,42,37
37
      DO 41
           J=1.NN
      II = J + 1
      DO 41 I=II.N
      DIF2=(B(I)-U(I))**2-(A(I)-U(I))**2
      DIF3=(B(J)-U(J))++2-(A(J)-U(J))++2
      P3=1.
      DO 40 K=1.N
      IF(K-I) 33,40,38
3 A
      IF(K-J) 39,40,39
39
      P3=P3%(B(K)-A(K))
40
      CONTINUE
      SUM2=SUM2+(H(I.J)+DIF2+DIF3+P3)
41
      CONTINUE
   42 Q=C*(P1+SUM1-SUM2/4.+TE1)
      TS2=0
      T$3=0
      TS4=0
      IF(N-1)65,65,66
   66 DO 67 I=1.N
      DO 67 J=1.N
      IF(J-I)69,67,69
      DSI=((B(I)-U(I))**4-(A(I)-U(I))**4)*((B(J)-U(J))**2-(A(J)-U(J))**2
     1)
      DS2=((B(I)-U(I))**3-(A(I)-U(I))**3)*((B(J)-U(J))**3-(A(J)-U(J))**3
     11
      = 2=1
      50 70 K=1.N
      IF (K-1)71,70,71
   71 IF (<-J)72,70,72
   72 P2=P2+(B(K)-A(K))
   70 CONTINUE
```

```
PAGE
       TS2=TS2+-(I+I)*H(I+J)*DS1*P2
       TS3=TS3+(H(I.I.)*H(J.J)+2.*H(I.J)**2)*DS2*P2
    67 CONTINUE
       TS2=TS2/15.
       TS3=TS3/72.
       IF(N-2)65,65,73
    73 DO 74 I=1.N
       DO 74 J=1.N
       IF(J-1)75,74,75
    75 DO 74 K=1.N
       IF(K-I)76,74,76
    76 IF(K-J)77,74,77
    77 DS1=(B(I)-U(I))**3-(A(I)-U(I))**3
       DS1=DS1*((B(J)-U(J))**2-(A(J)-U(J))**2)
       DS1=DS1*((B(K)-U(K))**2-(A(K)-U(K))**2)
       P2=1
       DO 78 L=1.N
       IF(L-1)79,78,79
    79 IF(L-J)80,78,80
    80 IF(L-K)81,78,81
    81 P2=P2*(B(L)-A(L))
    78 CONTINUE
       TS4=TS4+(2.*H(I.I)*H(J.K)+4.*H(I.J.)*H(I.K))*DS1*P2
    74 CONTINUE
       TS4=TS4/96.
    65 Q=Q+C*(TS2+TS3+TS4)
 C
 C
     CALCULATE C'
       CP=P1 +C
 C
     START RANDOM PROCESS
 C
     CALCULATE X (RANDOM VECTOR)
       FSUM=0.0
       F5Q=0.
       FGSUM=0.
       FGSQ=0.
       COFG=0.
    50 DO 59 NNN=1.100
       DO 51 I=1.N
       CALL RANDU(IX, IY, YFL)
        IX=IY
. 51
        X(I)=YFL
        DO 52 I=1.N
 52
        Y(I)=A(I)+X(I)*(B(I)-A(I))
 C
 C
      CALCULATE F AND G
 C
        DO 53 I=1.N
        XBR([]=0.
        DO 53 J=1.N
  53
        XBR(I)=XBR(I)+F(I,J)*(Y(J)-U(J))
        T=1.
        DO 54 I=1.N
        T=T*EXP(-.5*XBR(I)**2)
```

```
PAGE
       FF=T+C3
       * < 1 = 1
      DC 55 1=1.N
      SUMD=SURD+H(I,I)*(Y(I)-U(I))**2
      TS0=750-4'[:[)*+2*(Y([)-U([))**4
      ى ن≥شائىيىق
      IF(N-1) 58,58,56
       00 57 L=1.NN
      [M=U+1
      DO 57 I=IM.N
      SUM4=SU/4+((I)U+((L)U+((L,I)H+)/(I)))
57
      DO 82 1=1,N
      50 82 J=1.N
         J-1)23,82,83
   83 DI1=(Y(I)-U(I))**3*(Y(J)-U(J))
      DI2=(Y(I)-U(I))**2*(Y(J)-U(J))**2
      TS2=TC2+(4.#H(I.1)*H(I.J)*DI1+(H(I.I)*H(J.J)+2.*H(I.J)**2)*DI2)
   82 CONTINUE
      IF (N-2)84,84,85
   85 DO 56 1=1.N
      DO 86 J=1.N
      IF (J-I)87.86.87
   87 DO
         36 K=1.N
      IF (K-1)88,85.88
   88 IF(K-J)89,86,89
   89 DI1=(Y(I)-U(I)) ++2+(Y(J)-U(J))+(Y(K)-U(K))
      TS3=TS3+(2.*H(I,I)*H(J,K)+4.*H(I,J)*H(I,K))*DI1
   86 CONTINUE
   84 CONTINUE
   58 G=CP*(1.-.5*(SUM3+2.*SUM4)+.125*(TS1+TS2+TS3))
      FSUM=FSUM+FF
      FSG=F3Q+(FF**2)
      FGSUM=FGSUM+(FF-G)
      FGSQ=FGSQ+((FF-G)**2)
      COFG=COFG+FF*(FF-G)
57
      CONTINUE
      FM=FSUM/NT
     VAR1=(FSQ-(FSUM**2/NT))/(NT-1)
     COF=(COFG-FSUM*FGSUM/NT)/(NT-1.)
     SF=SCRT(VAR1/NT)
     FGM=FGSUM/NT
     VARZ= (FGSQ-(FGSUM**2)/NT)/(NT-1)
     SFG=SGRT(VAR2/NT)
     FG=FGM+D
     IF (SFG-ERROR)63,63,60
  60 IF(SF-ERROR)62,62,61
  61 NT=NT+100
     GO TO 50
  62 WRITE(3,100)FM.SF
     GO TO 1
  63 COF=COF/SGRT(VAR1*VAR2)
     WRITE(3,104)FG,SFG,COF
     GO TO 1
```

	SUPROUTINE LOCII.J.	IR.N.M.MS)			
	IX = I				· · · - · · · · · · · · · · · · · ·
	L=XL				
10	IF(MS-1) 10.20.30 IRX=N*(JX-1)+IX				
10	GO TO 36				
2.0	:F(:X-JX) 22,24,24				
2 ?	IRX=IX+(JX+JX-JX)/2	•			
24	GO TO 36 !RX=UX+([X*!X+!X)/2				•
	GO TO 35				
3 0	IRX=0				
	IF(IX-JX) 36,32,36				
32 35	IRX=IX IR=IRX			•	
פכ	RETURN				
· <u>······························</u>	END				
				·	
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	SUBROUTINE MSTRIA.R.	N. MSA. MSR.		
	DIMENSION A(1) .R(1)			
	DO 20 I=1.N		•	
	DO 20 J=1 • N			
5	IF(MSR) 5,10,5 IF(I+J) 10,10,20			
10	CALL LOC(I+J+IR+N+N+)	wca i		
10	IF(IR) 20,20,15	357/		
15	R(IR)=0.0			
• -	CALL LOC(I+J+IA+N+N+	MSAI		•
	IF(IA) 20.20.18			
18	R(IR)=A(IA)	-		
20	CONTINUE			
	RETURN			
	END			
			* *	
				
				1

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SUPPORTINE MINVIA - NODAL - MI
    DIRENSION A(1),L(1),M(1)
    5=1.0
    00 -0 K=1.N
    ٠ ﴿ ٤ ۽ ﴿ * ا
    スズニハイチく
    9:61=4(44)
    00 20 U=K.N
    12=84(1-1)
    00 20 1=K.N
    IU=.2-1
 10 IF(AB3(BIGA)-ABS(A(IJ)))15.20.20
 15 SI3A≈2((J)
    L(<)=1
    ダイベリョン
20 CONTINUE
    じゃし(人)
    IF(J=()35,35,25
25 KI= <- N
    DO 30 I=1.N
    KI=KI+N
   HOLD=-A(KI)
   JI=KI-K+J
   A(KI)=A(JI)
30 A(JI) =+0LD
35 I=M(X)
   IF(I-<)45,45,38
38 JP=N*(I-1)
   DO 40 J=1.N
   リベ=バドナ
   U+9U=16
   HOLD=-A(JK)
   A(JK) = A(JI)
40 A(JI)=HOLD
45 IF(BIGA)48,46,48
46 D=0.0
   RETURN
48 DO 55 I=1,N
   IF(I-K)50,55,50
50 IK=4K+I
   A(IK)=A(IK)/(-BIGA)
55 CONTINUE
   DO 65 :=1.N
   IK= < + I
   HOLD=A(IK)
   IJ= [-8;
   DO 65 J=1.N
   N+LI=LI
   :F(!-<)60,65,60
63 IF(J-K)62,65,62
62 KU=1U-1+K
  A(IJ)=HOLD*A(KJ)+A(IJ)
65 CONTINUE
   KU=K-N
   DO 75 J=1.N
                                     34
```

SUPPRISON SITE OF CONVERSION DIMENSION SITE OF CONVERSION TEST TYPE OF CONVERSION TEMPORED TO 0000-120							
NI=N-1 C IFST TYPE OF CONVERSION			SUBROUTINE ARR	AYIMODE . I . J . N	•M•5•D1		
C TEST TYPE OF CONVERSION IF: VODE+1) 100:100:120 C CONVERT FROM SINGLE TO DOUBLE DIMENSION 100 110 K=1:J NM=NW-NI 00 110 L=1:I 1J=1J-1 N"=NM=1 110 D(NM)=S(IJ) GO TO 140 C CONVERT FROM DOUBLE TO SINGLE DIMENSION 120 IJ=0 NM=0 00 130 K=1:J DO 125 L=1:I IJ=IJ+1 NM=NM+1 125 S(IJ)=D(NM) 130 NM=NM+NI 140 RETURN				•D(1)	,		
IF: VODE=1) 100.100.120 C							
C CONVENT FROM SINGLE TO DOUBLE DIMENSION 100	: :	<u> </u>					
10	*				•		
NM=N*J+1		C	CONVERT FROM SIN	IGLE TO DOUBLE	DIMENSION		,
DC 110 K=1,J NM=NM=NI DO 110 L=1,I IJ=IJ=1 NM=NM=1 110 D(NM)=5(IJ) GO TO 140 C CONVERT FROM DOUBLE TO SINGLE DIMENSION 120 IJ=0 NM=0 DC 130 K=1,J DO 125 L=1,I IJ=IJ+1 NM=NM+1 125 S(IJ)=D(NM) 130 NM=NM+NI 140 RETURN		: 22					
NM = NV = NI SO 110 L = 1 • I IJ = IJ = 1 NM = NM = 1 110 D(NM) = 5(IJ) GO TO 140 C CONVERT FROM DOUBLE TO SINGLE DIMENSION 120 IJ = 0 NM = 0 DO 130 K = 1 • J DO 125 L = 1 • I IJ = IJ + 1 NM = NM + 1 125 S(IJ) = D(NM) 130 NM = NM + NI 140 RETURN	2						
SO 110 L=1+I	j.		DO 110 K=1.J				•
			MARMA-MI				
N'=NM-1			00 110 L=1.I		The state of the s		
110 D(NM)=S(IJ) GO TO 140 C CONVERT FROM DOUBLE TO SINGLE DIMENSION 120 IJ=0 NM=0 DO 130 K=1.J DO 125 L=1.I IJ=IJ+1 NM=NM+1 125 S(IJ)=D(NM) 130 NM=NM+NI 140 RETURN	ă,		IJ=IJ-1				1 mg 100
GO TO 140 C CONVERT FROM DOUBLE TO SINGLE DIMENSION 120	es.		N'ASMM-1				
C CONVERT FROM DOUBLE TO SINGLE DIMENSION 120	,	110	D(NM)=5(IJ)			•	
120 IJ=0 NM=0 DO 130 K=1.J DO 125 L=1.I IJ=IJ+1 NM=NM+1 125 S(IJ)=D(NM) 130 NM=NM+NI 140 RETURN	. • . 		GO TO 140				
120 IJ=0 NM=0 DO 130 K=1.J DO 125 L=1.I IJ=IJ+1 NM=NM+1 125 S(IJ)=D(NM) 130 NM=NM+NI 140 RETURN		c	CONVERT FROM DOL	BLE TO SINGLE	DIMENSION		
NM=0 DC 130 K=1.J DC 125 L=1.I IJ=IJ+1 NM=NM+1 125 S(IJ)=D(NM) 130 NM=NM+NI 140 RETURN		120					
DO 125 L=1.I IJ=IJ+1 NM=NM+1 125 S(IJ)=D(NM) 130 NM=NM+NI 140 RETURN			NM=0			F 100	
DO 125 L=1.I IJ=IJ+1 NM=NM+1 125 S(IJ)=D(NM) 130 NM=NM+NI 140 RETURN			DO 130 K=1.J				
IJ=IJ+1							
NM=NM+1 125 S(IJ)=D(NM) 130 NM=NM+NI 140 RETURN	ŭ.						
125 S(IJ)=D(NM) 130 NM=NM+NI 140 RETURN	30						
130 NM=NM+NI 140 RETURN	: -	125					
140 RETURN							
				• •			
	.,						
	i de			-			
						il ili eran derjest desemble era	
							

		SUBROUTINE MESDIA+N+EF	PS+IER)	
		DIMENSION A(1)		
	C	TEST ON WRONG INPUT PARA IF(N=1) 12.1.1	MAMETER N	• .
:	1	IER=0		
1	ċ	INITIALIZE DIAGONAL LOCE	n n n n n n n n n n n n n n n n n n n	-
		KPIV=0	· ·	-
		DO 11 K=1•N		
•		KPIV=KPIV+K		
		IND=KPIV		
		LEND=K-1		
•	C	CALCULATE TOLERANCE	en e	
-		TOL=ABS(EPS*A(KPIV))		
1	C	START FACTORIZATION LOOP	OP OVER K-TH ROW	
1		DO 11 I=K+N		
		DSUM=0.		•
:	С	IF(LEND) 2+4+2 START INNER LOOP	y Marine Company of the Company of t	
	2	DO 3 L=1.LEND		
		LANF=KPIV-L		
		LIND=IND-L		A ju
1	3	DSUM=DSUM+A(LANF) *A(L)	LIND)	
	C	END OF INNER LOOP		•
	C	TRANSFORM ELEMENT A(IND))	
<u> </u>	4	DSUM=A(IND)-DSUM		
		IF(I-K) 10.5.10		
1	C		FELEMENT AND FOR LOSS OF SIGNIFICANCE	
ļ	5	IF(DSUM-TOL) 6.6.9		<u> </u>
	6	IF(DSUM) 12,12,7	نے دیاں دیست کی در ان میں شہرہ میست میں میں در انسان میں میں میں انسان کی انسان میں انسان کی انسان کی انسان کی	
	8	IF(IER) 8,8,9	e tree to a section of the section o	
-	°	IER=K-1 COMPUTE PIVOT ELEMENT		
	9	DPIV=SQRT(DSUM)		
		A(KPIV)=DPIV		
		DPIV=1./DPIV		
		GO TO 11		· 1 -
	C	CALCULATE TERMS IN ROW		
	17	A(IND)=DSUM*DPIV		•
	11	IND=IND+I		
_	<u> </u>	END OF DIAGONAL LOOP		
		RETURN	en e	
	12	IER=+1	· ····································	
—		RETURN		
-		END		
1				•
-				
-	•	•	and the second of the second o	
			en e	
_				

DIMENSION	A+N+EP\$+IER) (1+1) (1)/2 (IPIV)	
CALL MESO IF(IER) 9 I IPIV=N*(N	A+N+EP\$+IER) (1+1) (1)/2 (IPIV)	
<u> </u>	111/2 (IPIV)	
IPIV=N*(N	1)/2 (IPIV)	
110-1014	IPIV)	
	IPIV)	
00 6 [=1.	IPIV)	
DIN=1.0/A	IN CONTRACTOR OF THE PROPERTY	
G=(VI9I)A		
> 1 N=N	·	
1-1=CN3>		
LAME=N-KE	ND	•
[F(KEND)	5,5,2	
2 J=1ND		
DO 4 K=1.	KEND	and the second of the second o
₩ORK=0.0		
VIN=MIN-1		
LHOR=IPIV		
LVER=J		
DO 3 L=LA	NF.MIN	
LVER=LVER	_	en e
LHOR=LHOR		
	FA(LVER) #A(LHOR)	
FOW-=(L)A	(*DIN	man kan ing kananganggan kanggan kangg
4 J=J-MIN		
5 IPIV=IPIV	-MIN	
6 IND=IND-1		$(1 + 1)^{-1} = \frac{1}{2} + \frac{1}{2} = \frac{1}{2} =$
DO 3 I=1:		
IPIV=IPIV	+ I	TO THE PARTY OF THE CONTROL OF THE C
J=IPIV		e de la la la la compansament qua como de la compansament de la compan
DO 8 K=I	<u> </u>	
WORK=0.0		
LHOR=J		
DO 7 L=K		
LVER=LHOR		and the second s
_	+A(LHOR)*A(LVER)	e e e e e e e e e e e e e e e e e e e
7 LHOR=LHOR		
A(J)=WORK		
8 J=J+K		
9 RETURN		
END	a a carrier pro the second annual contraction of the second contractio	
	and the second of the second o	

```
SUBROUTINE CAL (THETA .PTS .AXIS)
                             DIMENSION A(5,2).S(5,5).BP(6).B(6).PTS(2).AXIS(2).KN(5).KI(5)
   10
                             READ(2+100) ((A(I+J)+J=1+2)+I=1+5)
   100
                             FORMAT(10F6.2)
                             WRITE(3,101) ((A(I,J),J=1,2),I=1,5)
   101
                             FORMAT(//+' THE POINTS ARE'+/+5(2x+'('+2F7+2+' )'+))
                             OC 1 I=1.5
                              S(I_{\bullet}I) = A(I_{\bullet}I) **2.
                              S(I+2)=A(I+1)+A(I+2)
                              S(I,3)=A(I,2)##2
                              S(I,4) = A(I,1)
1
                              S(I,5)=A(I,2)
                              CALL MINVIS,5, DU, KN, KI)
                              DO 2 1=1.5
                              SUM=0.0
                              DO 3 J=1,5
    3
                              SUM=SUM+S(I.J)*(-1.)
    2
                              B(I)=SUM
                              B(6) = 1.0
                              X=B(2)/(B(1)-B(3))
                               T = ATAN(X)/2
                              BP(1)=B(1)*(COS(T))**2.+B(2)*(SIN(T)*COS(T))+B(3)*(SIN(T))**2.
                              BP(2)=0.
                              BP(3)=B(1)*(SIN(T))**2-B(2)*SIN(T)*COS(T)+B(3)*(COS(T))**2.
                               BP(4) = B(4) * COS(T) + B(5) * SIN(T)
                              BP(5) = B(5) * COS(T) - B(4) * SIN(T)
                               BP(6) = B(6)
                               THETA=-T
                              D = (2 \cdot 49(1) + \cos(T) + B(2) + \sin(T) + (2) + B(3) + \cos(T) - B(2) + \sin(T) - (-2) + B(3) + \cos(T) + B(3) + B(3) + \cos(T) + B(3) 
                           1(1)*SIN(T)+B(2)*COS(T))*(2.*B(3)*SIN(T)+B(2)*COS(T))
                               PTS(1) = ((-B(4) + COS(T) - B(5) + SIN(T)) + (2 + B(3) + COS(T) - B(2) + SIN(T)) - (B(4) + COS(T) - B(5) + SIN(T)) + (B(5) + COS(T) - B(5) + SIN(T) + (B(5) + COS(T) - B(5) + SIN(T)) + (B(5) + COS(T) - B(5) + SIN(T) + (B(5) + COS(T) - B(5) + SIN(T)) + (B(5) + COS(T) - B(5) + SIN(T) + (B(5) + COS(T) - B(5) + SIN(T)) + (B(5) + COS(T) - B(5) + COS(T) - B(5) + (B(5) 
                           1(4)*SIN(T)-B(5)*COS(T))*(2.*B(3)*SIN(T)+B(2)*COS(T)))/D
                               PT5(2)=((2*#B(1)*COS(T)+B(2)*SIN(T))#(B(4)*SIN(T)-B(5)*COS(T))-(-2
                           1.*B(1)*SIN(T)+B(2)*COS(T))*(-B(4)*COS(T)-B(5)*SIN(T)))/D
                               Y=BP(3)*(BP(4)**2)+BP(1)*(BP(5)**2)=4**BP(1)*BP(3)*BP(6)
                               F=A95(8(1))
                                G=ABS(B(3))
                                IF(F-G) 20,20,21
    20
                                AXIS(1)=Y/(4.*(BP(1)**2)*BP(3))
                                AXIS(2)=Y/(4.*(BP(3)**2)*BP(1))
                                GO TO 24
    21
                                AXIS(2)=Y/(4.*(BP(1)**2)*BP(3))
                                AXIS(1)=Y/(4.*(BP(3)**2)*BP(1))
    24
                                AXIS(1)=SQRT(AXIS(1))
                                AXIS(2)=SQRT(AXIS(2))
                                RETURN
                                END
```